# Facile Regeneration Vitreous Microfibrous Entrapped Supported ZnO Sorbent with High Contacting Efficiency for Bulk H<sub>2</sub>S Removal from Reformate Streams in Fuel Cell Applications

Bong-Kyu Chang, Yong Lu, Hongyun Yang, and Bruce J. Tatarchuk

(Submitted January 16, 2006; in revised form May 22, 2006)

In this study, a microfibrous carrier consisting of 3 vol.% of 8  $\mu$ m (diameter) glass fibers is used to entrap 45 vol.% of 150 to 250  $\mu$ m (diameter) SiO<sub>2</sub> support particulates. ZnO is then nanodispersed onto the support by impregnation at the loading of 17 wt.%. At equivalent bed volumes, ZnO/SiO<sub>2</sub>-entrapped materials provide twofold longer breakthrough times for H<sub>2</sub>S (with a 67% reduction in sorbent loading) compared with packed beds of 1 to 2 mm commercial extrudates. Five-log reductions in H<sub>2</sub>S concentration with up to 75% ZnO utilization at breakthrough are achieved. H<sub>2</sub>S concentrations from 60 to 2000 parts per million in volume (ppmv) can be reduced to as little as 0.6 ppmv at 400 °C in 30% H<sub>2</sub>O at a face velocity of 1.7 cm/s for layers as thin as 1.0 mm. At 500 to 600 °C, ZnO/SiO<sub>2</sub>-entrapped materials provide much higher regenerability in air than do 1 to 2 mm commercial extrudates. The use of glass fibers permits greater than 50 regeneration cycles.

**Keywords** fuel cell, glass fiber, H<sub>2</sub>S removal, sorbent

## 1. Introduction

A significant challenge facing fuel cell applications is the development of on-site multistep reformation technologies utilizing high-energy density commercial-grade hydrocarbon fuels (Ref 1-4).

Microfibrous media technology developed at Auburn University (Ref 5-12) provides a novel approach for the more effective design of small, efficient, and lightweight fuel processors. A microfibrous media carrier, with large surface-tovolume ratios, can be used to entrap microsized sorbent and/or catalyst particulates while withstanding considerable shaking and avoiding bypassing. This generic approach can also enhance heat/mass transfer, improve contacting efficiency, and promote regenerability (Ref 13-15). The fabrication of the microfibrous media is based on reliable, proven, high-speed, rollto-roll papermaking and sintering processes, substantially reducing production costs while improving product quality. Microfibrous entrapped 16% Ni/Al<sub>2</sub>O<sub>3</sub> catalysts for toluene hydrogenation in a trickle bed reactor have demonstrated two to six times higher specific activities than the conventional packed bed catalysts on a gravimetric basis, while volumetric activities of 40 vol.% composite catalysts were 80% higher than those of conventional extrudates (Ref 13). Bulk H<sub>2</sub>S re-

This paper was presented at the ASM Materials Solutions Conference & Show held October 18-21, 2004 in Columbus, OH.

**Bong-Kyu Chang, Yong Lu, Hongyun Yang,** and **Bruce J. Tatarchuk**, Center for Microfibrous Materials Manufacturing (CM<sup>3</sup>), Department of Chemical Engineering, Auburn University, Auburn, AL 36849. Contact e-mail: schummc@auburn.edu. moval is a key step in the fuel processing in ensuring the activity of various cleanup catalysts and high-value membrane electrode assemblies. To accomplish this goal, in the current study a sintered glass fiber carrier, with high contacting efficiency, was used to entrap microsized  $ZnO/SiO_2$  sorbent particulates for regenerable continuous batch bulk  $H_2S$  removal. Microfibrous media preparation, characterization, and evaluation will be discussed as well as the impact of performance behavior on reactor weight, volume, and bed utilization efficiency.

# 2. Experimental

#### 2.1 Fabrication of Glass Fiber-Entrapped ZnO/SiO<sub>2</sub> Sorbent

Sintered glass fiber-entrapped (GFE) 150 to 250 µm (diameter) SiO<sub>2</sub> (300 m<sup>2</sup>/g; Grace Davison) support particulates were fabricated by a regular wet layer paper-making/sintering procedure (Ref 5-12). ZnO was then placed onto the supports by incipient wetness impregnation. A total of 6 g of 8 µm (diameter)  $\times$  6 mm (length) S-2 glass fiber chops (Advanced Glassfiber Yarns LLC), and 0.7 g of 30 to 60 µm (diameter) cellulose (100-1000 µm in length) were added into 2.5 L of water and stirred vigorously at 50 Hz for 2 min. The produced suspension and 24 g of  $SiO_2$  (which can be increased up to 36 g) were added into the headbox of the 15.2 cm (diameter) circular sheet former and stirred to a uniform suspension. The 15.2 cm circular preform was then formed by draining, pressing at ~400 kN/m, and drying in air at ~110 °C. The as-prepared preform was directly sintered in air for 30 min at 925 °C while burning off the celluloses. The sintered GFE SiO<sub>2</sub> particulates were composed of 3.0 vol.% of 8 µm (diameter) glass fibers, 45 vol.% of 150 to 250 µm (diameter) SiO<sub>2</sub> particulates, and 52 vol.% of voidage. To place the ZnO onto the support, asprepared microfibrous entrapped SiO<sub>2</sub> paper was immersed

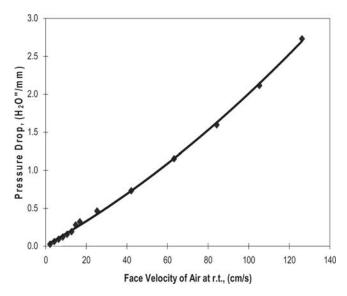


Fig. 1 The pressure drop of the GFE  $ZnO/SiO_2$  as a function of the face velocity of air at room temperature

into a ZnO sol-gel for 10 min. The paper was subsequently removed from the ZnO sol-gel, drained under vacuum, and calcined in air for 20 min at each of the selected temperatures (80, 100, 120, 140, 160, and 180 °C). The final composite sorbent has a ZnO loading of 17 wt.% (including the mass of the glass fibers). The ZnO sol-gel was prepared by adding 70 mL of  $NH_3$ · $H_2O$ , 42 g of  $(NH_4)_2CO_3$ , and 66 g of Zn(Ac)<sub>2</sub>· $GH_2O$  into 56 mL of water and stirring vigorously. The pressure drop of the GFE ZnO/SiO<sub>2</sub> as a function of the face velocity of air at room temperature is shown in Fig. 1.

A commercial ZnO sorbent (4.8 mm pellet; 25  $m^2/g$ ; 90 wt.% ZnO) from Sud Chemie was crushed and sieved into the desired particle size for comparative studies.

#### 2.2 Characterization

Powder x-ray diffraction (XRD) patterns were recorded using a scanning speed of  $4^{\circ}$ /min and an accelerating voltage of 40 kV, unless stated otherwise.

The scanning electron microscopy (SEM) micrographs of the GFE ZnO/SiO<sub>2</sub> sorbent were obtained by a Zeiss DSM 940 instrument. As shown in Fig. 2, the micron-sized ZnO/SiO<sub>2</sub> particulates were uniformly entrapped into a well-sinter-locked, three-dimensional network of 8  $\mu$ m glass fibers.

#### 2.3 Microreactor Evaluation

Absorption and regeneration cycle tests were carried out in a continuous batch mode. The sorbent loading was kept at 0.53 mL (16.5 mm [diameter] × 2.5 mm [thickness]). To avoid the gas bypass, a sample of GFE ZnO/SiO<sub>2</sub> sorbent was cut into a 16.5 mm (diameter) disc and sealed with the inner wall of the tubular quartz reactor by a mixture of  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> powder and SiO<sub>2</sub> sol-gel (Si-RIG, 40 wt.% SiO<sub>2</sub>, Zircar Ceramics). Absorption with an H<sub>2</sub>S challenge of 60 ppmv in a model reformate stream (40% CO<sub>2</sub>, 10% CO, 9% C1-C3 hydrocarbon, with balance being H<sub>2</sub>) was performed at 400 °C in the presence of 30% H<sub>2</sub>O at a face velocity of 1.7 cm/s on a dry gas basis (dry gas flow rate 220 mL [at standard temperature and pressure]/min). The H<sub>2</sub>O vapor of 30% was added into the model reformate due to the need to perform downstream

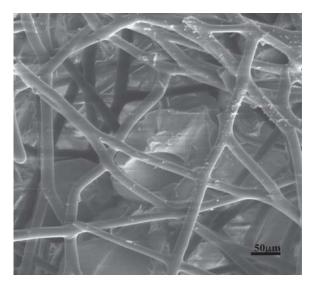


Fig. 2 SEM micrographs of GFE ZnO/SiO<sub>2</sub> sorbents

Table 1 Results of absorption with 60 ppmv  $H_2S$  challenge in a model reformate at 400°C and 1.7 cm/s face velocity in the presence of 30% steam over GFE ZnO/SiO<sub>2</sub> sorbents and 1 to 2 mm commercial sorbent extrudates

Sorbent	GFE ZnO/SiO <sub>2</sub>	1-2 mm commercial extrudates
Total mass, g	0.2	0.55
ZnO content, mg	34	495
Bed volume, mL	0.53	0.53
BT, min(a)	540	180
ZnO utilization at BT, %	75	1.8

GHSV = 24,900 h (not including the  $H_2O$ ). (a) Breakthrough time at 1 ppmv  $H_2S$  breakthrough

water-gas shift reaction (WGSR) and to keep the membrane electrolyte assembly from drying in practical operations. Regeneration was performed at 500 to 600 °C in an airflow (50 mL/min) for 1 to 3 h. The breakthrough of H<sub>2</sub>S is determined by the rate of color change of the lead acetate strips (H<sub>2</sub>S detection limit; 1 ppmv). To prove that the equilibrium  $H_2S$ absorption is achieved in the current study, a MultiRAE Plus multigas monitor (PMG-50/5P, H<sub>2</sub>S detection limit 0.5 ppmv) was used to monitor the outlet H<sub>2</sub>S concentrations continuously. Absorption with H<sub>2</sub>S challenges of 60 and 2000 ppmv in He ran at 400 °C in the presence of 30% H<sub>2</sub>O. Helium was used in lieu of the model reformate because H<sub>2</sub> and CO are interferential to the H<sub>2</sub>S detection of the MultiRAE monitor. When using He, the outlet  $H_2S$  concentrations were ~0.5 ppmv before 1 ppmv  $H_2S$  breakthrough, consistent with the equilibrium  $H_2S$ concentration (~0.6 ppmv) at 400 °C in 30% H<sub>2</sub>O.

#### 3. Results and Discussion

The absorption with a H<sub>2</sub>S challenge of 60 ppmv in a model reformate at 400 °C in 30% H<sub>2</sub>O was studied over both GFE ZnO/SiO<sub>2</sub> and 1 to 2 mm commercial extrudates. The results are summarized in Table 1. At an equivalent bed volume, GFE ZnO/SiO<sub>2</sub> sorbent provided about twofold longer breakthrough

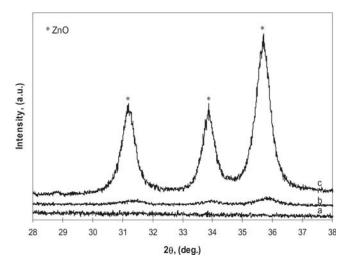


Fig. 3 XRD patterns of (a) GFE  $SiO_2$ , (b) GFE  $ZnO/SiO_2$ , and (c) Sud Chemie extrudates

times for H<sub>2</sub>S with 67% reduction of the sorbent loading, compared with a packed bed of 1 to 2 mm commercial extrudates. ZnO utilization was 75% for ZnO/SiO<sub>2</sub> entrapped materials, which is 14-fold higher than that of 1 to 2 mm commercial extrudates.

The XRD patterns of GFE ZnO/SiO<sub>2</sub> sorbent and commercial extrudates for H<sub>2</sub>S absorption are presented in Fig. 3. The commercial extrudate sample afforded relatively sharp XRD peaks of ZnO crystals, corresponding to a crystal size of 17 nm. In addition, the commercial extrudate sample has a N2-BET surface area of  $\sim 25 \text{ m}^2/\text{g}$  (provided by manufacturer). This suggests that most ZnO crystals were buried inside the bulk, which in turn causes the poor accessibility of ZnO. In comparison, very weak and broad XRD peaks of ZnO were observed on the ZnO/SiO<sub>2</sub>-entrapped materials, corresponding to a crystal size of ~5 nm. The N<sub>2</sub>-BET surface area of the  $ZnO/SiO_2$ -entrapped materials was determined to be 250 m<sup>2</sup>/g. This indicates that the nanosized ZnO was highly dispersed onto the pore surface of entrapped SiO<sub>2</sub> supports. It is wellunderstood that H<sub>2</sub>S absorption with large commercial extrudates is a typical process, in which both the reaction and regeneration rates are controlled by intraparticle and lattice diffusions (Ref 15).

For GFE ZnO/SiO<sub>2</sub> sorbents, the nanodispersed nature of the ZnO combined with the use of small-sized support particulates not only attenuates lattice and intraparticle diffusion limits, but also promotes high contacting efficiency and high accessibility of the ZnO. These beneficial properties, therefore, create high ZnO utilization and high bed utilization efficiency (Table 1).

One other obvious advantage of the nanodispersed nature of the ZnO and the use of small-sized support particulates is the great improvement of the regenerability at 500 to 600 °C in air.

Under parallel regeneration conditions, the microfibrous sorbent provided up to 10-fold higher reactivity recovery percentage after regeneration in air from 500 to 600 °C for 1 to 3 h compared with the packed bed of 1 to 2 mm commercial extrudates. The higher regeneration temperature and longer time period of regeneration made a higher reactivity recovery

percentage. To reveal the nature of this large difference in regenerability, XRD analyses were carried out on spent samples before and after regeneration at 500 to 600 °C in air. The spent samples were collected when the outlet  $H_2S$  concentration reached 60 ppmv (the same as inlet concentration).

## 4. Conclusions

A highly void, tailorable sintered glass-fiber carrier has been fabricated via wet-layer papermaking/sintering technology (Ref 5-12). This carrier can be used, with high surface-tovolume ratios, to entrap microsized catalyst/sorbent particulates while withstanding considerable shaking, avoiding bypassing, maintaining low-pressure drop, and achieving excellent corrosion resistance with structural integrity.

A carrier consisting of 3 vol.% glass fibers was used to entrap 45 vol.% 150 to 250  $\mu$ m ZnO/SiO<sub>2</sub> H<sub>2</sub>S sorbent particulates for the regenerable use. The nanodispersed nature of the ZnO combined with the use of small support particulates not only promotes high ZnO utilization, high contacting efficiency, and high accessibility of ZnO, but also facilitates the regeneration in air at 500 to 600 °C, compared with the packed bed of 1 to 2 mm commercial extrudates. In addition, the use of glass fibers permits a large number of absorption/ regeneration cycles due to their high corrosion resistance and thermal stability. The above-noted approach allows the continuous batch H<sub>2</sub>S removal from reformate streams while significantly increasing the bed utilization efficiency and reducing overall system weight and volume.

#### Acknowledgment

Financial support from the U.S. Army (DASG 60-00-C-0070) is gratefully acknowledged.

#### References

- 1. T. McCreedy, Trends Anal. Chem., 2000, 19, p 396
- S. Srinivasan, I.M. Hsing, P.E. Berger, K.F. Jensen, S.L. Firebaugh, M.A. Schmit, M.P. Harrold, J.J. Lerou, and J.F. Ryley, *AIChE J.*, 1997, 43, p 3059
- K. Watanabe, M. Sakairi, H. Takahashi, K. Takahiro, S. Nagata, and S. Hirai, J. Electrochem. Soc., 2001, 148, p B473
- 4. X. Wu, D. Weng, L. Xu, and H. Li, Surf. Coat. Technol., 2001, 145, p 226
- B.J. Tatarchuk, M.F. Rose, A. Krishnagopalan, J.N. Zabasajja, and D. Kohler, U.S. Patent 5 304 330, 1994; U.S. Patent 5 080 963, 1992
- R.A. Overbeek, A.M. Khonsari, Y.-F. Chang, L.L. Murrell, B.J. Tatarchuk, and M.W. Meffert, U.S. Patent 6 231 792, 2001
- B.J. Tatarchuk, U.S. Patent 5 096 663, 1992; U.S. Patent 5 102 745, 1992
- 8. D.R. Cahela and B.J. Tatarchuk, Catal. Today, 2001, 69, p 33-39
- C.J. Marrion, D.R. Cahela, S. Ahn, and B.J. Tatarchuk, J. Power Sources, 1994, 47, p 297-302
- D.A. Kohler, J.N. Zabasajja, A. Krishnagopalan, and B.J. Tatarchuk, J. Electrochem. Soc., 1990, 137(1), p 136-141
- 11. S. Ahn and B.J. Tatarchuk, J. Appl. Electrochem., 1997, 27, p 9-17
- 12. M.W. Meffert, Ph.D. Thesis, Auburn University, 1998
- D.K. Harris, D.R. Cahela, and B.J. Tatarchuk, Composites, *Appl. Sci. Manufact.*, 2001, **32A**(8), p 1117-1126
- Y. Lu and B.J. Tatarchuk, presented at 226th American Chemical Society National Meeting (New York, NY), Sept 2003, CATL-042; AIChE 2003 National Meeting (San Francisco, CA), Nov 2003, p 331b
- 15. M.V. Twigg, Catalyst Handbook, 2nd ed., London: Wolfe, 1989, p 209